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<b>(21) International Application Number:</b> PCT/US90/02189 <b>(22) International Filing Date:</b> 23 April 1990 (23.04.90) <b>(30) Priority data:</b> 349,612 10 May 1989 (10.05.89) US <b>(71) Applicant:</b> EXXON CHEMICAL PATENTS INC. [US/US]; 1900 East Linden Avenue, Linden, NJ 07036-0710 (US). <b>(72) Inventor:</b> HENDEWERK, Monica, Louise ; 5006 Loch Lomond, Houston, TX 77096 (US). <b>(74) Agents:</b> KURTZMAN, Myron, B. et al.; Exxon Chemical Company, P.O. Box 5200, Baytown, TX 77522-5200 (US).		<b>(81) Designated States:</b> AT (European patent), BE (European patent), CA, CH (European patent), DE (European patent), DK (European patent), ES (European patent), FR (European patent), GB (European patent), IT (European patent), JP, KR, LU (European patent), NL (European patent), SE (European patent).  <b>Published</b> <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>
<b>(54) Title:</b> POLYPROPYLENE COMPOSITION AND METHOD FOR FUNCTIONALIZATION OF POLYPROPYLENE  <b>(57) Abstract</b> <p>The present invention relates to a process for the functionalization, and preferably the maleation of a polyolefin, preferably polypropylene, by use of a selected class of peroxides which will not cause the molecular weight of the polyolefin to significantly degrade. The class of peroxide initiators which are capable of successful use in the present invention may be more broadly classified as peroxides which have radical fragments when the peroxide is dissociated, which are a combination of R. and RO., where R is an aliphatic hydrocarbon, and O is oxygen. The preferred peroxide initiators for use in carrying out the present invention so as to obtain the results indicated above are t-butyl peroxyvalate and isononanoyl peroxide. The composition resulting from the practice of the process of the invention is a maleated polypropylene in which the polypropylene has more than 0.3 weight percent grafted maleic anhydride and preferably greater than 0.4 weight percent, for example, from 0.4 to 4 weight percent or more grafted maleic anhydride on the polymer chains and in which the MFR is less than 100.</p>		

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POLYPROPYLENE COMPOSITION AND METHOD FOR FUNCTIONALIZATION  
OF POLYPROPYLENE

1        This invention relates to a new functionalized polypropylene  
2 composition and a new and improved process for the  
3 functionalization of polypropylene, particularly the maleation of  
4 polypropylene.

5                Brief Description of the Prior Art

6        To prepare polypropylene for certain end-use applications it  
7 is necessary to functionalize the polymer, i.e., to incorporate  
8 functional groups such as maleic anhydride onto the polypropylene  
9 polymer chains. The reaction of maleic anhydride with  
10 polypropylene is well known in the art. Examples of the prior art  
11 are U.S. Patent Nos. 4,404,312; 4,506,056; 3,414,551; 4,370,450;  
12 and 4,639,495. European Patent application 0 225 186 is another  
13 example of a method of grafting maleic anhydride onto  
14 polypropylene. In the prior art, the maleation of polypropylene  
15 has been accomplished by the use of free radical initiators such  
16 as a peroxide initiator to induce maleation. However, the prior  
17 art peroxides which have been used for functionalizing  
18 polypropylene cause substantial degradation of the molecular  
19 weight of the maleated polypropylene. In an attempt to avoid  
20 molecular weight degradation of the maleated polypropylene the  
21 prior art methods employed low levels of peroxide initiator. See,  
22 for example, U.S. Patent No. 4,404,312 which states that the  
23 organic peroxide should not be more than about 0.1 percent by  
24 weight, and preferably not more than 0.01 percent by weight of the  
25 polypropylene to be reacted. As a result, in the prior art, the  
26 extent of maleation of the polypropylene has been restricted.  
27 Other attempts to avoid the molecular weight degradation require  
28 the use of a third ingredient, such as styrene, which becomes a  
29 part of the polymer, or require the use of a catalyst such as  
30 N,N-dialkylethanolamine, or other nitrogen, phosphorus, or sulfur

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1 containing compounds. Examples of such ingredients are found in  
2 U.S. Patent No. 4,506,056 and EPO Application 0 225 186.

3 Summary of the Invention

4 The present invention is a novel composition wherein the  
5 molecular weight of a functionalized polypropylene product is  
6 greater than heretofore obtained with the prior art radical  
7 initiators, and a novel functionalization process wherein minimal  
8 molecular weight degradation of the polypropylene occurs during a  
9 radical initiated functionalization process. This is accomplished  
10 by the use of a selected class of peroxides which have been found  
11 to produce significant grafting of unsaturated monomers useful for  
12 functionalizing polypropylene, such as maleic anhydride, himic  
13 anhydride, acrylic acid, methacrylic acid, vinyltrimethoxysilane,  
14 acrylamide, itaconic acid, maleic acid, fumaric acid, monomethyl  
15 maleate, monoethyl maleate, fumaric anhydride, vinyl amines and  
16 amides, and other substituted vinyl monomers that are capable of  
17 free radical polymerization, onto polypropylene without causing  
18 significant molecular weight degradation of the polypropylene.

19 Polypropylene has many attractive characteristics such as a  
20 high melting temperature, low density, chemical inertness and low  
21 cost. However, in order to use polypropylene in applications such  
22 as adhesives, coextrudable tie layers for multilayer composites,  
23 metal coatings, and polymer blends, it is necessary to chemically  
24 modify polypropylene to incorporate a reactive moiety onto the  
25 backbone of the polymer. As a primary advantage of the present  
26 invention, one can employ high levels of peroxide and obtain a  
27 polymer composition having a high molecular weight with a  
28 significant level of functionality which can be made into film or  
29 otherwise processed by extrusion, fiber spinning, etc. In  
30 contrast, the lower molecular weight functionalized polypropylene  
31 produced by conventional approaches generally cannot be so used or  
32 processed.

33 A further advantage of the present invention is that the  
34 molecular weight degradation of polypropylene can be controlled,  
35 independent of the level of grafting of maleic anhydride onto the  
36 polypropylene, through variation in temperature, time and other  
37 process variables. In the prior art, molecular weight degradation

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1 increases when increasing amounts of peroxides are used to  
2 increase grafting.

3 The process of this invention does not require the presence of  
4 a catalyst, additive, or process modifier (third ingredient) as  
5 disclosed in U.S. 4,506,056 to prevent molecular weight  
6 degradation. The functionalized polypropylene compounds produced  
7 with the process of this invention have a melt flow rate (MFR) of  
8 one hundred (100) or less, (measured by ASTM Standard F 1238-86),  
9 but preferably seventy-five (75) or less. The peroxide initiators  
10 preferred for use in practice of the process have a short  
11 half-life ( $t_{1/2}$ ) at 180°C, preferably less than 3 seconds at  
12 180°C, and the peroxide initiator decomposes to produce radical  
13 fragments in combinations of either  $R\cdot$  or  $RO\cdot$ , wherein R is an  
14 alkyl group, preferably a  $C_1$ - $C_{30}$  alkyl group. When the  
15 radical is  $RO\cdot$ , R is most preferably t-butyl. The energy for  
16 bonding a hydrogen atom to these types of radicals is about 105  
17 Kcal/mol or less. The peroxides preferred for use in the process  
18 are t-butyl peroxyvalate or isononanoyl peroxide.

19 Brief Description of the Drawings

20 Figure 1 is a graph of the melt flow rate (MFR) versus the  
21 weight percent of maleic anhydride incorporated for maleated  
22 polypropylene compositions produced by using dicumyl peroxide, a  
23 typical peroxide used in radical initiated grafting processes,  
24 compared to a maleated polypropylene composition produced by  
25 either of two preferred embodiments of the process of the present  
26 invention, one embodiment being a melt phase process (B) and the  
27 second embodiment being a solid phase process (C).

28 Figure 2 is a graph of the melt flow rate (MFR) of a  
29 functionalized polypropylene versus the amount of peroxide  
30 initiator used to produce the functionalized polypropylene  
31 composition, for a functionalized polypropylene produced using  
32 dicumyl peroxide in accordance with prior art processes (D) and  
33 for a functionalized polypropylene produced using t-butyl  
34 peroxyvalate in accordance with the process of this invention  
35 (E).

36 Detailed Description of the Invention

37 The present invention relates to a process for the

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1 functionalization, and preferably the maleation of a polyolefin,  
2 preferably polypropylene, by use of a selected class of peroxides  
3 which will not cause the molecular weight of the polyolefin to  
4 significantly degrade. While the differences between  
5 polypropylene and its copolymers are recognized, the term  
6 "polypropylene" as used in the claims includes both homopolymers  
7 and copolymers of propylene for the sake of convenience. The  
8 process of this invention does not require the presence of a  
9 catalyst, additive, or process modifier to prevent molecular  
10 weight degradation.

11 The functionalizing agent employed in the process of this  
12 invention may be any of the unsaturated monomers conventionally  
13 used to functionalize a polyolefin. Such functionalizing agents  
14 include, for example, carboxylic acids such as acrylic and  
15 methacrylic acid; acid anhydrides such as maleic and himic  
16 anhydride; acid amides such as acrylamide; and vinyl siloxanes  
17 such as vinyltrimethoxysilane. The functionalizing agent  
18 preferred for use in the process shall be described and  
19 illustrated with reference to the functionalization of  
20 polypropylene by reaction with maleic anhydride (MAH). Although  
21 the invention will be described with reference to maleic  
22 anhydride, it should be understood that functionalizing reagents  
23 different from maleic anhydride, such as the unsaturated monomers  
24 previously identified, can be employed in the practice of this  
25 invention. Accordingly, the term "maleation" or "maleated" as  
26 used hereafter should be understood to mean "functionalization"  
27 insofar as the use of functionalizing reagents other than maleic  
28 anhydride are contemplated for use in the process of the invention.

29 The composition resulting from the practice of the process of  
30 the invention is a maleated polypropylene in which the  
31 polypropylene has on the average more than 0.3 weight percent  
32 (0.13 mole %) grafted maleic anhydride and preferably greater than  
33 0.4 weight percent (0.17 mole %) grafted maleic anhydride, and an  
34 MFR of less than 100. The mole % most preferably is in the range  
35 of 0.13-1.71.

36 The melt flow rate (MFR) of the maleated polypropylene,  
37 measured by ASTM Standard E1238-8, is about one hundred (100) or

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1 less, preferably less than 75, and most preferably less than 60.  
2 These values can be compared with the prior art as in Table 2  
3 where it is demonstrated that the use of peroxides typically used  
4 in the prior art produces maleated polypropylenes with MFR's  
5 greater than 300. Maleated polypropylene made by the prior art  
6 methods with an MFR of less than 100 contain very low levels of  
7 grafted maleic anhydride, as demonstrated by the overlapping area  
8 of the curves in Figure 1 in the region of very low weight percent  
9 grafted maleic anhydride, low MFR. In accordance with this  
10 invention in which polypropylene does not significantly degrade,  
11 the MFR of the maleated polypropylene product is related to the  
12 MFR of the initial polypropylene polymer. The advantage of the  
13 composition of this invention is that the maleated polymer product  
14 can be made into films or can be processed by extrusion, fiber  
15 spinning, etc., and used in engineering plastic applications  
16 whereas the lower molecular weight functionalized polymers  
17 produced by prior art functionalization processes generally have  
18 MFR's much greater than 100 and cannot be so processed.

19 In carrying out the process of the present invention, the  
20 maleic anhydride and peroxide reagents should be mixed with the  
21 polypropylene preferably before the polypropylene is heated, and  
22 most preferably the maleic anhydride and the peroxide free radical  
23 initiator should be mixed prior to adding such mixture to the  
24 polypropylene. Although use of a solvent is not required for  
25 mixing the reagents with polypropylene, using an inert, low  
26 molecular weight, volatile solvent, such as pentane, hexane, or  
27 other hydrocarbons, or methylethyl ketone, acetone, or other low  
28 molecular weight species, or any other suitable liquid, to coat  
29 the polymer with the reagents, does improve the mixing of the  
30 reagents and improve the dispersion of the reagent mixture on the  
31 polypropylene when so used. The mixture of peroxide initiator and  
32 maleic anhydride is added to the polypropylene to coat the polymer  
33 with such components of the mixture. If a solvent is used as a  
34 coating and dispersion aid for the reagents, after the mixture is  
35 coated onto the polypropylene the solvent is evaporated from the  
36 polymer, leaving the maleic anhydride and peroxide reagents on the  
37 surface of the polypropylene.

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1       Thereafter, the polymer with the reagents present is treated  
2 in one of two ways.

3       A preferred mode for conducting the reaction of maleic  
4 anhydride with polypropylene is in the melt phase mode wherein the  
5 temperature exceeds 160°C. In accordance with this embodiment, a  
6 high level of grafting with minimal molecular weight degradation  
7 is obtained. In accordance with this mode, the polypropylene is  
8 mixed with the peroxide and maleic anhydride or coated by  
9 evaporation of inert diluent from a slurry of peroxide/maleic  
10 anhydride. Typical diluents are pentane, heptane, methyl, ethyl,  
11 ketone and the like. Thereafter, the reagent coated polypropylene  
12 granules or pellets are heated in a vessel such as a Brabender  
13 plasticorder, an autoclave, an extruder or other equipment of like  
14 purpose or are reacted in a fluidized bed or gas phase reactor.  
15 Good results are obtained at temperatures of about 180-250°C, but  
16 preferably 180-220°C. The longer the time that the polypropylene  
17 is subjected to the reaction temperature, namely the preferred  
18 temperature of 180-220°C, the greater will be the amount of  
19 grafted maleic anhydride, without further degrading the molecular  
20 weight of the polypropylene.

21       An alternative method for conducting the maleation reaction is  
22 in the particulate or solid phase, at a temperature below the  
23 melting point of the polypropylene, namely at a temperature of  
24 less than about 165°C. In accordance with this mode, the closer  
25 to 165°C the better the grafting results obtained. The MFR of  
26 maleated polypropylene products produced in the particulate phase  
27 is less than fifty (50) but most commonly less than ten (10) when  
28 starting with a polypropylene resin having an MFR of 3. The  
29 longer the time that the polypropylene is subjected to the  
30 reaction temperature, namely the preferred temperature of  
31 150-165°C, the greater will be the amount of the grafted maleic  
32 anhydride, without further degrading the molecular weight of the  
33 polypropylene.

34       Alternatively, in either the melt phase or solid phase mode,  
35 the maleic anhydride and the select peroxide can be added to the  
36 polypropylene separately. Addition of the maleic anhydride  
37 separately from the peroxide results in lower grafting levels, but



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1 maintains the advantage of insignificant molecular weight  
2 degradation of the polymer product.

3 Since in the process of the present invention the molecular  
4 weight of the polypropylene is not significantly degraded, the  
5 amount of the peroxide used, based on the quantity of  
6 polypropylene to be reacted, may be as high as 10 mole percent,  
7 calculated as the number of moles of peroxide per mole of  
8 propylene monomer units ( $C_3H_6$  units) present. The preferred  
9 amounts of the peroxide initiator are in the range of about 0.14  
10 to 6 mole percent.

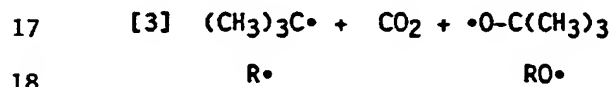
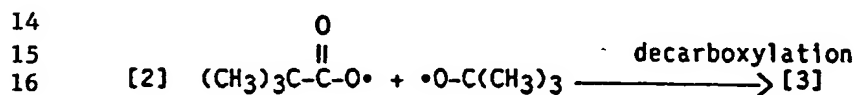
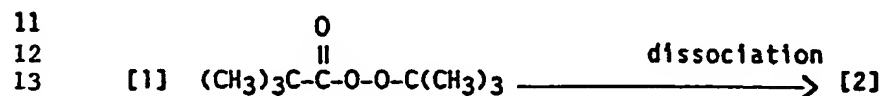
11 The presence of a catalyst, additive, or other process  
12 modifier during reaction is not required in order to accomplish  
13 the objectives of the present invention, namely, the grafting of  
14 substantial quantities of maleic anhydride to polypropylene  
15 without significant degradation of the polypropylene molecular  
16 weight. However, such catalysts, additives, or other process  
17 modifiers can be included in this reaction to obtain similar  
18 results as given in the prior art for other processes using other  
19 peroxides (EPO Patent Application 0 225 186). As above mentioned,  
20 it is generally desirable in this invention to use a minor amount  
21 of a low molecular weight hydrocarbon or other solvent to enhance  
22 the mixing of the reagents and to disperse the reagent mixture on  
23 the polypropylene.

24 With the process of the present invention the maleated  
25 polypropylene produced will have an MFR of one hundred (100) or  
26 less, i.e., from 0 to 100, and desirably 0-75, and most desirably  
27 0-60, indicating that the molecular weight of the maleated  
28 polypropylene product is much higher than the prior art polymers  
29 of polypropylene with equivalent amounts of maleic anhydride  
30 grafted using peroxide initiators. Also, in accordance with this  
31 invention the amount of maleic anhydride grafted is greater than  
32 0.3 weight percent and preferably greater than 0.4 weight percent  
33 grafted maleic anhydride with an MFR of less than 100 which  
34 distinguishes the present invention from the prior art.

35 The preferred peroxide initiators for use in carrying out the  
36 present invention so as to obtain the results indicated above are  
37 t-butyl peroxyvalate and isononanoyl peroxide. The class of

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1 peroxide initiators which are capable of successful use in the  
 2 present invention may be more broadly classified as peroxides  
 3 which have radical fragments when the peroxide is dissociated,  
 4 which are a combination of R• and RO•, where R is an aliphatic  
 5 hydrocarbon, and O is oxygen. Such radical fragments exist (1)  
 6 when the peroxide separates at the two oxygen atoms in the middle  
 7 of the peroxide (dissociation), or (2) when the fragments formed  
 8 by dissociation undergo decarboxylation or beta-scission after  
 9 separation at the two oxygen atoms in the middle of the peroxide.  
 10 The dissociation pathway for t-butyl peroxyvalate is:




19 It has been found that the hydrogen bond energy, i.e the  
 20 energy gained by adding a hydrogen radical (H•) to a peroxide  
 21 radical (P•):



23 can be related to whether the peroxide initiator will function in  
 24 the present invention. Table 1 shows the hydrogen bond energy and  
 25 conversely the radical stability for various free radicals or  
 26 radical fragments which may exist after a peroxide dissociates.

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TABLE 1

Radical Type	Approximate Hydrogen Bond Energy	Radical Reactivity (Hydrogen Abstraction)
$\text{C}_6\text{H}_5\text{O}^\bullet$ or $\text{C}_6\text{H}_5\text{O}-\text{O}^\bullet$	112 Kcal/mol	Most Reactive
$\text{RO}^\bullet$	105 Kcal/mol	
$\text{H}_3\text{C}^\bullet$	104 Kcal/mol	
$\text{RCH}_2^\bullet$	98 Kcal/mol	
$\text{R}_2\text{CH}^\bullet$	95 Kcal/mol	
$\text{R}_3\text{C}^\bullet$	91 Kcal/mol	
		Least Reactive

Peroxides which dissociate into free radicals with a hydrogen bond energy of about 105 Kcal/mol and below, and which have a short half life at 180°C are most satisfactory for the purposes of the present invention, namely, producing a functionalized polypropylene, particularly a maleated polypropylene, with minimal degradation of its molecular weight.

EXAMPLES

In the examples and tables which follow, the quantities of reagents employed and the properties of resulting compositions were determined as follows:

The melt flow rate (MFR) of the starting polymer and of the maleated polymer product were determined in accordance with ASTM Standard D1238-86, i.e., a melt temperature of 230°C and a load of 2.16 Kg.

The amount of maleic anhydride (MAH) used for reaction with a polymer is reported as weight percent MAH. The weight percent MAH was calculated as the number of grams of maleic anhydride present per gram of polymer multiplied by 100.

The molar concentration of peroxide used, as reported in the

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1 examples and tables, was calculated as the number of moles of  
2 peroxide per mole of monomer units in the polymer being reacted.  
3 Wherein polypropylene was the polymer reacted (Examples 1 to 23)  
4 the molar concentration of peroxide used was calculated as the  
5 ratio of the moles of peroxide to the moles of propylene monomer  
6 units ( $C_3H_6$ , M.W. = 42 g/mole) present in the polymer.  
7 Wherein an ethylene-propylene copolymer was the polymer reacted  
8 (in Examples 23-27) the molar concentration of peroxide used was  
9 calculated as the ratio of moles of peroxide to the sum of the  
10 moles of propylene and ethylene monomer units ( $C_3H_6$ , M.W. = 42  
11 g/mole;  $C_4H_4$ , M.W. = 28 g/mole) present.

12 To determine the amount of maleic anhydride grafted onto the  
13 polymer, the maleated polymer was dissolved in xylene then  
14 precipitated from solution with acetone, filtered and dried. All  
15 samples in the examples were treated in this fashion. The weight  
16 percent of maleic anhydride grafted to the polymer was then  
17 determined by Fourier Transform Infrared (FTIR) analysis. FTIR  
18 films were pressed at 230°C for several minutes. The maleic  
19 anhydride concentrations grafted to the polymer were calculated  
20 from the intensity of the peak appearing between 1782-1790  $cm^{-1}$ .  
21 The FTIR was calibrated by oxygen analysis performed on maleated  
22 polypropylene and maleated ethylene-propylene rubber samples. The  
23 molecular weight of the grafted polymer was monitored by measuring  
24 the melt flow rate (MFR) using ASTM Standard D1238-86 and by Gel  
25 Permeation Chromatography (GPC).

26 The amount of maleic anhydride and peroxide reagents used and  
27 their relative concentration, as well as the temperature chosen,  
28 the time of reaction, the MFR or molecular weight of the polymer  
29 starting material, and the method of addition of the reagents to  
30 the polymer starting material were chosen to illustrate the  
31 variety of desired results that may be achieved by varying such  
32 conditions in the practice of the process of this invention. The  
33 examples which follow are illustrative of such variations, but are  
34 not intended to limit or otherwise exclude other combinations of  
35 such parameters.

36 Specific examples of peroxide initiators which are  
37 unsatisfactory and those which are satisfactory in carrying out

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1 the present invention are given below as Examples 1-11  
2 (comparative) and Examples 12-13 (inventive). Table 2, following  
3 Example 13, shows data obtained for the various peroxide  
4 initiators utilized in Examples 1-13. Examples labelled with a  
5 "C" are comparative examples.

6 Example 1-C

7 The reaction of isotactic polypropylene having a melt flow  
8 rate (MFR) of 3.0 and maleic anhydride in the presence of a  
9 peroxide initiator was carried out in a Brabender plasticorder.  
10 One hundred forty-four milligrams (144 mg) of dicumyl peroxide  
11 (0.07 mole percent) was mixed with 1.6 g maleic anhydride (5  
12 weight percent) at room temperature in the powder form and then  
13 mixed with 32 grams of polypropylene granules. The Brabender  
14 plasticorder was brought to a temperature of 180°C and rotated at  
15 30 rpm. While rotating at 30 rpm, the powdered peroxide-maleic  
16 anhydride-polypropylene mixture was added to the Brabender  
17 plasticorder after which the speed of the Brabender was increased  
18 to 60 rpm. The polymer mixture was blended for 10 minutes at  
19 180°C, then removed from the Brabender. The results are  
20 summarized in Table 2.

21 Example 2-C

22 The procedure of Example 1 was followed except that 0.14 mole  
23 percent dicumyl peroxide (288) mg was used. The results are  
24 summarized in Table 2.

25 Example 3-C

26 The procedure of Example 1 was followed except that 0.24 mole  
27 percent dicumyl peroxide (0.48 g) was used. The results are  
28 summarized in Table 2.

29 Example 4-C

30 The procedure of Example 1 was followed except that 0.31 mole  
31 percent dicumyl peroxide (0.64 g) was used. The results are  
32 summarized in Table 2.

33 Example 5-C

34 The procedure of Example 1 was followed except that 0.47 mole  
35 percent dicumyl peroxide (0.96 g) was used. The results are  
36 summarized in Table 2.

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1 Example 6-C

2 The procedure of Example 1 was followed except that 0.62 mole  
3 percent dicumyl peroxide (1.3 g) was used. The results are  
4 summarized in Table 2.

5 Example 7-C

6 The procedure of Example 1 was followed except that 0.78 mole  
7 percent dicumyl peroxide (1.6 g) was used. The results are  
8 summarized in Table 2.

9 Example 8-C

10 The procedure of Example 1 was followed except that 4.05 grams  
11 of dicumyl peroxide (1.75 mole percent) 3.6 grams of maleic  
12 anhydride (10 weight percent MAH) and 36 grams of polypropylene  
13 were used. The results are summarized in Table 2.

14 Example 9-C

15 The reaction of isotactic polypropylene having a MFR of 3.0  
16 and maleic anhydride in the presence of a peroxide initiator was  
17 carried out in a Brabender plasticorder. Maleic anhydride, 10  
18 weight percent, and 2,5-dimethyl-2,5-di(t-butylperoxy) hexane  
19 (tradename Lupersol 101), 1.75 mole percent, were dissolved in  
20 methyl ethylketone at ambient temperature, then mixed with 36 g  
21 polypropylene granules. The solvent was then evaporated from the  
22 mixture to leave the peroxide and MAH reagents on the surface of  
23 the polypropylene granules. A brabender plasticorder was brought  
24 to a temperature of 180°C and rotated at 30 rpm. While rotating  
25 at 30 rpm, the peroxide-maleic anhydride-polypropylene mixture was  
26 added to the Brabender plasticorder after which the speed of the  
27 Brabender was increased to 60 rpm. The polymer mixture was  
28 blended for 10 minutes at 180°C, then removed from the Brabender.  
29 The results are summarized in Table 2.

30 Example 10-C

31 The procedure of Example 9 was followed except that 1.75 mole  
32 percent of t-butyl peracetate (3.6 g) was used as the peroxide  
33 initiator. The results are summarized in Table 2.

34 Example 11-C

35 The procedure of Example 9 was followed except that 1.75 mole  
36 percent of benzoyl peroxide (3.9 g) was used as the peroxide  
37 initiator. The results are summarized in Table 2.

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1 Example 12

2 The procedure of Example 9 was followed except that 1.61 mole  
3 percent of isononanoyl peroxide (7.2 g) was used as the peroxide  
4 initiator and 20 weight percent MAH was used. The polymer mixture  
5 was blended for five minutes at 210°C. The results are summarized  
6 in Table 2.

7 Example 13

8 The procedure of Example 9 was followed except that 1.75 mole  
9 percent of t-butyl peroxyvalate (3.6 g) was used as the peroxide  
10 initiator. The results are summarized in Table 2.

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Table 2.

EXP. No.	REACTANTS					REACTION CONDITION S		POLYMER PRODUCT		PEROXIDE HALF LIFE, $t_{1/2}$ @ 180°C (seconds)*
	PEROXIDE	AMOUNT (mole%)	MAH wt%	INITIAL POLYMER TYPE	MFR	TEMP (°C)	TIME (min.)	GRAFTED Wt%	MFR	
1-C	dicumyl peroxide	0.07	5	isoPP*	3.0	180	10	0.2	42	23
2-C	dicumyl peroxide	0.16	5	isoPP	3.0	180	10	0.3	120	23
3-C	dicumyl peroxide	0.24	5	isoPP	3.0	180	10	0.5	130	23
4-C	dicumyl peroxide	0.31	5	isoPP	3.0	180	10	0.4	160	23
5-C	dicumyl peroxide	0.47	5	isoPP	3.0	180	10	0.7	>500	23
6-C	dicumyl peroxide	0.62	5	isoPP	3.0	180	10	0.8	>500	23
7-C	dicumyl peroxide	0.78	5	isoPP	3.0	180	10	1.6	>500	23
8-C	dicumyl peroxide	1.75	10	isoPP	3.0	180	10	1.6	>500	23
9-C	Lupersol 101	1.75	10	isoPP	3.0	180	10	1.6	>500	37
10-C	t-butyl peracetate	1.75	10	isoPP	3.0	180	10	1.1	380	9
11-C	benzoyl peroxide	1.75	10	isoPP	3.0	180	10	1.0	330	3
12	isonanoyl peroxide	1.61	20	isoPP	3.0	210	5	1.9	62	0.5
13	t-butyl per- oxypivalate	1.75	10	isoPP	3.0	180	10	1.6	32	0.25

\*isoPP = isotactic polypropylene



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1 Table 2 vividly illustrates that the MFR of the polymers  
2 maleated in accordance with the preferred process of this  
3 invention using preferred peroxide initiators, such as t-butyl  
4 peroxyvalerate and isononanoyl peroxide are well below one hundred  
5 (100) demonstrating that minimal molecular weight degradation  
6 occurs with peroxide initiators which satisfy the criteria set  
7 forth for use in this invention, while still grafting significant  
8 amounts of maleic anhydride.

9 As illustrated by the contrast of Examples 12 and 13 with  
10 Examples 1-11, it is also important to the process of this  
11 invention that the peroxide initiators have a relatively short  
12 half-life at 180°C. The half-life values identified in Table 2  
13 for each peroxide were calculated using activation energies and  
14 rate constant data from the Polymer Handbook, 2nd Edition,  
15 Brandrup & Immergut. The two preferred peroxide initiators, for  
16 example, have a half-life of tenths of a second at 180°C. Once  
17 chosen, the peroxide initiators, with a half-life of less than  
18 about three seconds at 180°C, can be used at any temperature. A  
19 peroxide having a half-life of over a few seconds at 180°C will  
20 produce a maleated polypropylene product which has a significantly  
21 reduced molecular weight.

22 The following examples Nos. 14-22 illustrate the melt phase  
23 mode of maleation of polypropylene in accordance with the process  
24 of this invention.

25 Example 14

26 T-butyl peroxyvalerate as the peroxide initiator, maleic  
27 anhydride, and polypropylene pellets (MFR = 1.0) were added  
28 directly to the feed hopper of a single screw extruder-reactor and  
29 then passed into the feed zone of the extruder. The polymer  
30 passed through all zones of the reactor, held at 180°C, with an  
31 average residence time of 1.5 minutes. The amount of peroxide and  
32 maleic anhydride used, and the product MFR and MAH grafting level  
33 are shown in Table 3.

34 Examples 15-21

35 T-butyl peroxyvalerate as the peroxide initiator and maleic  
36 anhydride were dissolved in methyl ethylketone at ambient  
37 temperature, then mixed with polypropylene granules, MFR 3.0. The

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1 solvent was evaporated leaving the MAH and peroxide on the surface  
2 of the polymer. A Brabender plasticorder was brought to a  
3 temperature of 180°C and rotated at 30 rpm. While rotating at 30  
4 rpm the peroxide-maleic anhydride-polypropylene mixture was added  
5 to the Brabender plasticorder after which the speed of the  
6 Brabender was increased to 60 rpm. The polymer mixture was  
7 blended for 10 minutes at 180°C, then removed from the Brabender.  
8 The amount of peroxide and maleic anhydride used and the time of  
9 reaction varied and is reported for each example in Table 3 which  
10 follows.

11 Example 22

12 The procedure of Example 20 was followed except that the  
13 Brabender plasticorder was brought to a reaction temperature of  
14 200°C and the peroxide-MAH-polymer mixture was blended for only 2  
15 minutes. The results are reported in Table 3.

16 The following examples Nos. 23-25 illustrate the solid phase  
17 mode for maleation of polypropylene in accordance with the process  
18 of this invention.

19 Examples 23-25

20 Maleic anhydride and t-butyl peroxyphthalate (TBPP) as the  
21 peroxide initiator were dissolved in methyl ethylketone at ambient  
22 temperature, then mixed with polypropylene granules, MFR 3.0. The  
23 solvent was evaporated leaving the MAH and peroxide on the surface  
24 and in the pores of the polymer granules. The dry mixture of  
25 peroxide-MAH-polypropylene was added to an autoclave and the  
26 autoclave was purged with nitrogen for 15 minutes. The autoclave  
27 was evacuated to  $10^{-3}$  torr and then closed to external  
28 atmosphere. The autoclave was then heated to 150°C and stirred  
29 for a period of time after which its temperature was reduced to  
30 room temperature and it was returned to atmospheric pressure.  
31 The amount of peroxide and maleic anhydride used and the  
32 temperature and time of reaction for each example are summarized  
33 in Table 3.

Table 3.

EXP. No.	PEROXIDE	REACTANTS				REACTION CONDITIONS		POLYMER PRODUCT	
		AMOUNT (mole%)	MAH wt %	INITIAL POLYMER		TEMP (°C)	TIME (min.)	GRAFTED Wt %	MER
14	TBPP**	0.21	1	isoPP*	1.0	180	1.5	0.3	6
15	TBPP	0.89	5	isoPP	3.0	180	10	0.7	33
16	TBPP	1.75	10	isoPP	3.0	180	10	1.2	28
17	TBPP	4.40	25	isoPP	3.0	180	10	1.9	35
18	TBPP	5.30	30	isoPP	3.0	180	20	2.3	42
19	TBPP	0.89	5	isoPP	3.0	180	10	0.7	30
20	TBPP	2.67	15	isoPP	3.0	180	10	1.2	36
21	TBPP	4.42	25	isoPP	3.0	180	10	1.9	35
22	TBPP	4.42	25	isoPP	3.0	180	20	2.3	42
23	TBPP	2.67	15	isoPP	3.0	200	2	1.2	59
24	TBPP	2.67	30	isoPP	3.0	150	60	0.5	1.8
25	TBPP	2.67	20	isoPP	3.0	150	180	1.1	3.2
26	TBPP	2.67	20	isoPP	3.0	150	300	1.4	0.9

\* isoPP = isotactic polypropylene

\*\* TBPP = t-butyl peroxyphthalate

1        Table 3 demonstrates that parameters such as temperature,  
2 reaction time, apparatus type, and reagent concentration can be  
3 varied to control the level of grafting and molecular weight  
4 breakdown during PP functionalization. In particular it should be  
5 noted that when an enclosed apparatus such as an extruder is used  
6 (Example 14) a much lower quantity of reagents is required to  
7 obtain similar grafting results to the Brabender, which is open at  
8 the top.

9        The polymers useful in this invention include polypropylene  
10 and random or block copolymers of propylene with a lesser amount  
11 of one or more ( $C_2-C_{18}$ )  $\alpha$ -olefins and/or diolefins such as  
12 ethylene, butene, hexene, butadiene, hexadiene, and so on. Use of  
13 such copolymers results in even higher grafting levels and lower  
14 MFR levels than are achieved in the case of homopolypropylene.  
15 The lower MFR is achieved because, in addition to the elimination  
16 of molecular weight breakdown as described by this invention, some  
17 crosslinking occurs in the presence of a peroxide in a copolymer  
18 containing other olefins, such as ethylene. This crosslinking  
19 phenomenon is well known in the art. Example Nos. 26-32  
20 illustrate the application of this invention to copolymers of  
21 propylene with ethylene. The results of such examples are shown  
22 in Table 4.

23        Examples 26 through 29 illustrate melt phase maleation of  
24 ethylene-propylene copolymers using the process of this  
25 invention. Example 30 illustrates melt phase maleation of  
26 ethylene-propylene using prior art. The results are summarized in  
27 Table 4.

28        Example 26

29        An ethylene-propylene copolymer containing 3 weight percent  
30 ethylene was maleated in accordance with the process of the  
31 invention. Maleic anhydride and t-butyl peroxyphthalate (TBPP) as  
32 the peroxide initiator were dissolved in methyl ethylketone or  
33 pentane at ambient temperature, then mixed with polypropylene  
34 granules, MFR 3.0. The solvent was evaporated leaving the MAH and  
35 peroxide on the surface and in the pores of the polymer granules.  
36 A Brabender plasticorder was brought to a temperature of 180°C and  
37 rotated at 30 rpm. While rotating at 30 rpm the peroxide-maleic

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1 anhydride-polypropylene mixture was added to the Brabender  
2 plasticorder after which the speed of the Brabender was increased  
3 to 60 rpm. The polymer mixture was blended for 10 minutes at  
4 180°C, then removed from the Brabender.

5 Example 27

6 The procedure of Example 26 was followed except that the  
7 ethylene-propylene copolymer used contained 5 weight percent  
8 ethylene.

9 Example 28

10 The process and procedure of Example 14 (extruder reactor) was  
11 followed except that the polymer used was an ethylene-propylene  
12 copolymer.

13 Example 29

14 The process and procedure of Example 28 was followed except  
15 that the temperatures in the last 2 segments of the extruder were  
16 raised to 200°C and 220°C respectively.

17 Example 30-C

18 The process and procedure of Example 14 (extruder reactor) was  
19 followed except that the polymer used was an ethylene-propylene  
20 copolymer and the peroxide used was a 2,5-dimethyl-2,5-di  
21 (t-butylperoxy)hexene (tradename Lupersol 130). The results are  
22 summarized in Table 4.

23 Examples 31 and 32 illustrate the solid phase maleation of  
24 ethylene-propylene copolymers using the process of this invention.

25 Example 31

26 An ethylene-propylene copolymer containing 3 weight percent  
27 ethylene was maleated in accordance with the process of the  
28 invention. Maleic anhydride and t-butyl peroxyplvalate as the  
29 peroxide initiator were dissolved in methyl ethylketone or pentane  
30 at ambient temperature, then mixed with polypropylene granules,  
31 MFR 3.0. The solvent was evaporated leaving the MAH and peroxide  
32 on the surface and in the pores of the polymer granules. The dry  
33 mixture of peroxide-MAH-polypropylene was added to an autoclave  
34 and the autoclave was purged with nitrogen for 15 minutes. The  
35 autoclave was evacuated to  $10^{-3}$  Torr and then heated to 150°C.  
36 The contents were stirred for 60 minutes.

37 Example 32

Table 4.

EXP. No.	REACTANTS			INITIAL POLYMER		REACTION CONDITIONS		POLYMER PRODUCT	
	PEROXIDE	AMOUNT (m ole%)	MAH wt. %	TYPE	MER	TEMP (°C)	TIME (min.)	GRAFTED Wt. %	MER
20	TBPP**	2.67	15	isoPP*	3.0	180	10	1.2	36
26	TBPP	2.67	15	3% ethylene copolymer of PP	3.0	180	10	1.4	35
27	TBPP	2.67	15	5% ethylene copolymer of PP	3.0	180	10	2.0	23
28	TBPP	0.21	1	15% ethy- lene copolymer of PP	1.7	180	1.5	0.44	6
29	TBPP	0.21	1	15% ethy- lene copolymer of PP	1.7	180- 220	1.5	0.44	6
30-C	TBPP	0.21	1	15% ethy- lene copolymer of PP	1.7	180	2.5	0.49	540
23	TBPP	2.67	30	isoPP	3.0	150	60	0.50	1.8
31	TBPP	2.67	30	3% ethylene copolymer of PP	3.0	150	60	0.80	4
32	TBPP	2.67	30	5% ethylene copolymer of PP	3.0	150	60	1.7	0.5

\* isoPP = isotactic polypropylene

\*\* TBPP = t-butyl peroxy-pivalate

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1       The procedure of Example 26 was followed except that the  
2 ethylene-propylene copolymer used contained 5 weight percent  
3 ethylene. The results are summarized in Table 4.

4       Examples 31 and 32, conducted at 150°C show that significantly  
5 less molecular weight degradation occurs in the solid phase  
6 experiment than in the melt phase experiment. Comparison of  
7 Examples 26-28 with the previous examples demonstrates that the  
8 crosslinking affect achieved with the presence of ethylene  
9 monomeric units in the polypropylene polymer results in slightly  
10 lower MFR than when the crosslinking ability is not present  
11 (homopolypropylene). Concomitantly, the 5 percent ethylene  
12 copolymer exhibits the lowest MFR under the same maleation  
13 conditions.

14       The foregoing disclosure and description of the invention are  
15 illustrative and explanatory thereof, and various changes in the  
16 size, shape and materials, as well as in the details of the  
17 illustrated construction may be made without departing from the  
18 spirit of the invention.

CLAIMS:

1. A functionalized (co)polypropylene comprising:  
polypropylene having more than 0.13 mole percent grafted functional groups derived from substituted vinyl monomers that are capable of free radical polymerization, said functionalized polypropylene having an MFR of 100 or less.
2. The functionalized polypropylene of claim 1 wherein the vinyl monomer is one of an unsaturated acid, anhydride, amide, ester, or a siloxane.
3. The functionalized polypropylene of claim 1 having more than 0.17 mole percent grafted functional groups.
4. The functionalized polypropylene of claim 2 wherein the grafted functional groups are derived from maleic anhydride, himic anhydride, acrylic acid, methacrylic acid, vinyltrimethoxysilane, acrylamide, itaconic acid, maleic acid, fumaric acid, monomethyl maleate, monoethyl maleate, fumaric anhydride, vinyl amines and amides.
5. The functionalized polypropylene of claim 2 wherein the grafted functional groups are derived from an unsaturated anhydride.
6. The functionalized polypropylene of claim 5 wherein the anhydride is maleic anhydride.
7. The functionalized polypropylene of claim 6 having 0.13 - 1.71 mole percent grafted maleic anhydride.
8. The functionalized polypropylene of claim 1 derived from homopolypropylene.



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9. The functionalized polypropylene of claim 2 derived from a , copolymer or terpolymer of propylene with a lesser amount of one or more of a  $C_2$ - $C_{18}$   $\alpha$ -olefin or diolefin.
10. A free radical process for functionalizing polypropylene, comprising:
  - adding to polypropylene an unsaturated functionalizing agent and a free radical initiator wherein;
  - said unsaturated functionalizing agent is an acid, anhydride, amide or a siloxane; and
  - said free radical initiator is a peroxide producing radical fragments, selected from the group consisting of  $R\cdot$  and  $RO\cdot$ , where R is a  $C_1$  -  $C_{30}$  aliphatic hydrocarbon and O is oxygen; and
  - heating the polypropylene while in contact with said free radical initiator and said functionalizing agent at a temperature sufficient to graft the functionalizing agent to the polypropylene, whereby the polypropylene is functionalized with minimal molecular weight degradation.
11. The process of claim 10, wherein:
  - the initiator is a peroxide having a  $t_{1/2}$  of less than three seconds at 180°C.
12. The process of claim 11, wherein:
  - R is *t*-butyl when the radical fragment is  $RO\cdot$ .
13. The process of claim 12, wherein:
  - the peroxide initiator is isononanoyl peroxide.
14. The process of claim 11, wherein:
  - the peroxide initiator upon dissociation has one radical fragment with an alkoxy group, and another radical fragment with an alkyl group.

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15. The process of claim 14, wherein:  
the peroxide initiator is t-butyl peroxyphthalate.
16. The process of claims 13, 14 or 15, wherein:  
the functionalizing agent is maleic anhydride.
17. The process of claim 16, wherein:  
the polypropylene is heated to a temperature  
sufficient to melt the polypropylene so that the  
polypropylene is in the melt phase during the  
grafting reaction of the maleic anhydride to the  
polypropylene chain.
18. The process of claim 16, wherein:  
the polypropylene is heated to temperature  
insufficient to melt the polypropylene so that the  
polypropylene is in the solid phase during the  
grafting reaction of the maleic anhydride to the  
polypropylene chain.
19. The process of claim 16, wherein:  
the polypropylene is first heated, and the maleic  
anhydride and peroxide are added.
20. The process of claim 17, wherein:  
the temperature in the melt phase is from about the  
melt temperature of the polypropylene to about 250°C.
21. The process of claim 10, wherein:  
the amount of initiator present in the reaction with  
the polypropylene is equivalent to between about 0.14  
mole percent and 6 mole percent based on the number  
of moles of monomer present.
22. The process of claim 10, wherein:  
the resulting functionalized polypropylene has a melt  
flow rate of about one hundred (100) or less.

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23. The process of claim 10, wherein:  
the resulting functionalized polypropylene has an  
average of two or more functional groups for each  
polypropylene chain.
24. The product produced by the process of claim 10.
25. The product produced by the process of claim 12.
26. The product produced by the process of claim 21.
27. The product produced by the process of claim 22.
28. The product produced by the process of claim 23.

Figure 1

Melt Flow Rate vs. Wt.% Grafted MAH  
during grafting of Homopolypropylene

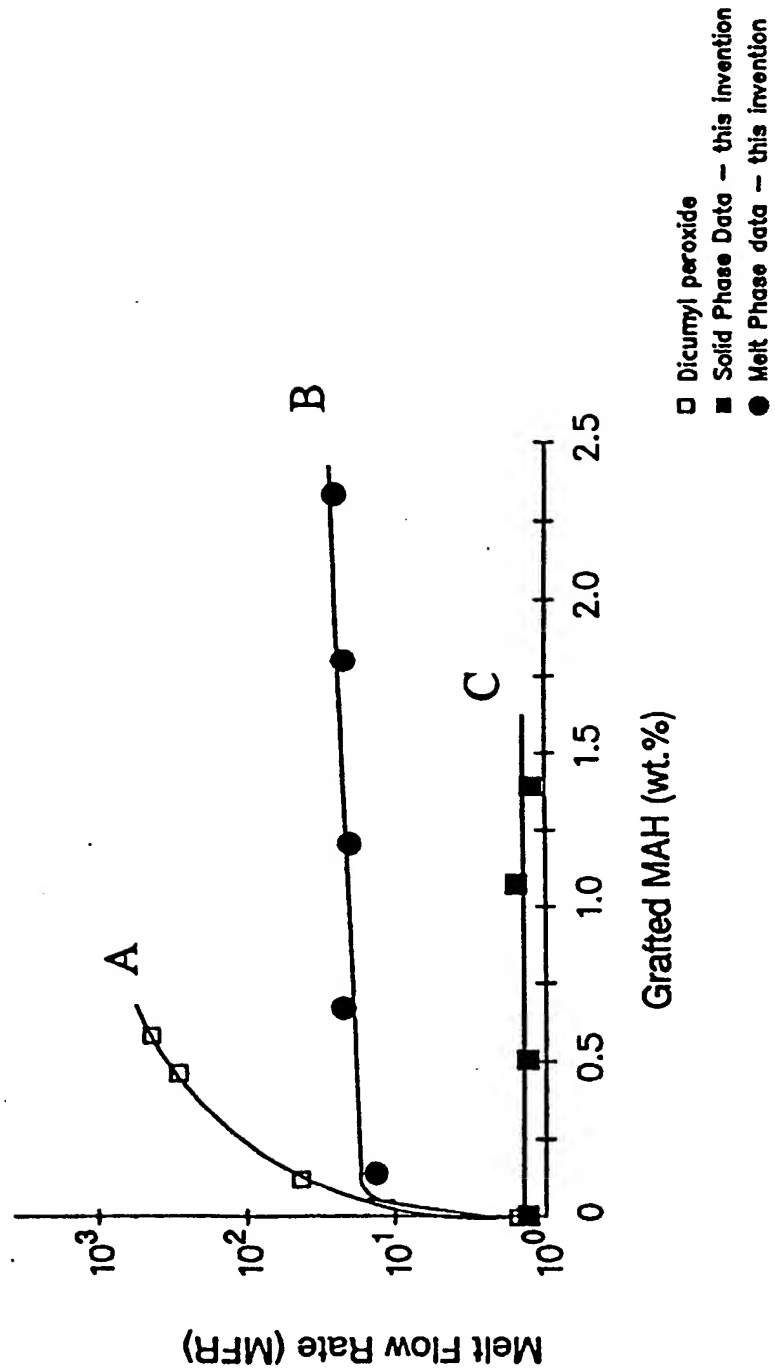
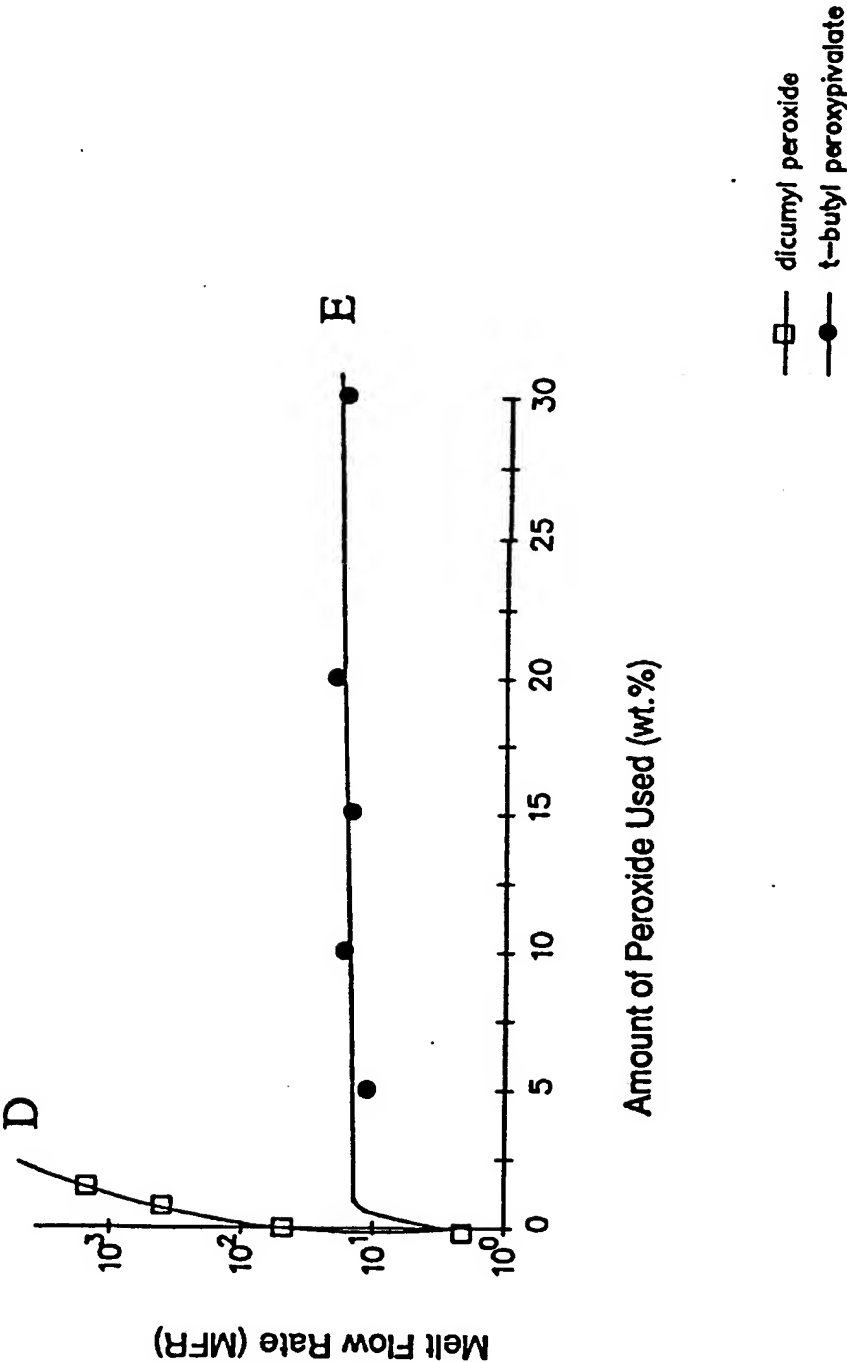


Figure 2  
The Effect of Peroxide on Melt Flow Rate  
during grafting of Homopolypropylene



# INTERNATIONAL SEARCH REPORT

International Application No PCT/US 90/02189

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (If several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC <sup>5</sup> : C 08 F 255/00, C 08 F 8/46		
<b>II. FIELDS SEARCHED</b>		
Minimum Documentation Searched *		
Classification System	Classification Symbols	
IPC <sup>5</sup>	C 08 F	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched *		
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT *</b>		
Category *	Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup>	Relevant to Claim No. <sup>13</sup>
Y	EP, A, 0134941 (DYNAMIT NOBEL) 27 March 1985 see claims 1-7  --	1-28
Y	FR, A, 2186490 (EASTMAN KODAK) 11 January 1974 see claims 1-8  --	1-28
Y	US, A, 4506056 (N.G. GAYLORD) 19 March 1985 see claim 1; column 4 (cited in the application)  --	1-28
A	FR, A, 2251611 (EASTMAN KODAK) 13 June 1975 see claims 1-4  --	1
<p>* Special categories of cited documents: <sup>10</sup></p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&amp;" document member of the same patent family</p>		
<b>IV. CERTIFICATION</b>		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
9th August 1990	17. 09. 90	
International Searching Authority	Signature of Authorized Officer	
EUROPEAN PATENT OFFICE	M. SOTELO	

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, " with indication, where appropriate, of the relevant passages	Relevant to Claim No.
A	US, A, 3755495 (A.E. SCHRAGE) 28 August 1973 see claims 1-8  --	1
A	EP, A, 0082704 (E.I. DU PONT DE NEMOURS) 29 June 1983 see claims 1-4. & US, A, 4639495 (cited in the application)  --	1
A	FR, A, 1482380 (HERCULES POWDER) 26 May 1967 see summary; page 2, column 1 & US, A, 3414551 (cited in the application)  -----	1

**ANNEX TO THE INTERNATIONAL SEARCH REPORT  
ON INTERNATIONAL PATENT APPLICATION NO.**

US 9002189  
SA 37026

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 07/09/90. The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

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		NL-A- 6607411	27-12-66
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